

CS 247 – Scientific Visualization

Lecture 26: Vector / Flow Visualization, Pt. 8

Markus Hadwiger, KAUST

Reading Assignment #15++



Read (optional):

- Tobias Günther, Irene Baeza Rojo:
Introduction to Vector Field Topology
<https://cgl.ethz.ch/Downloads/Publications/Papers/2020/Gun20b/Gun20b.pdf>
- Roxana Bujack, Lin Yan, Ingrid Hotz, Christoph Garth, Bei Wang:
State of the Art in Time-Dependent Flow Topology: Interpreting Physical Meaningfulness Through Mathematical Properties
<https://onlinelibrary.wiley.com/doi/epdf/10.1111/cgf.14037>
- B. Jobard, G. Erlebacher, M. Y. Hussaini:
Lagrangian-Eulerian Advection of Noise and Dye Textures for Unsteady Flow Visualization
<http://dx.doi.org/10.1109/TVCG.2002.1021575>
- Anna Vilanova, S. Zhang, Gordon Kindlmann, David Laidlaw:
An Introduction to Visualization of Diffusion Tensor Imaging and Its Applications
<http://vis.cs.brown.edu/docs/pdf/Vilanova-2005-IVD.pdf>

Quiz #4: May 5



Organization

- First 30 min of lecture
- No material (book, notes, ...) allowed

Content of questions

- Lectures (both actual lectures and slides)
- Reading assignments (except optional ones)
- Programming assignments (algorithms, methods)
- Solve short practical examples

Lagrangian vs. Eulerian

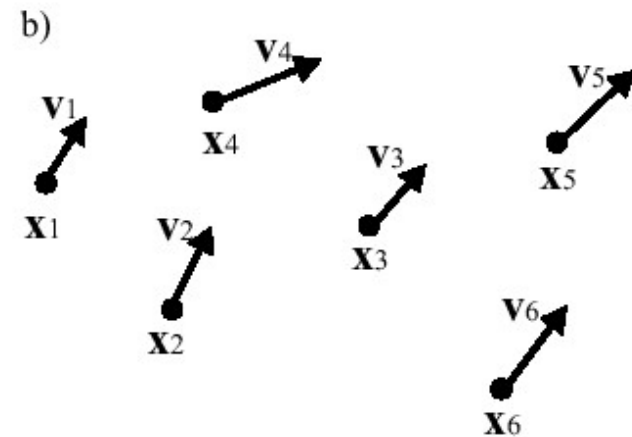
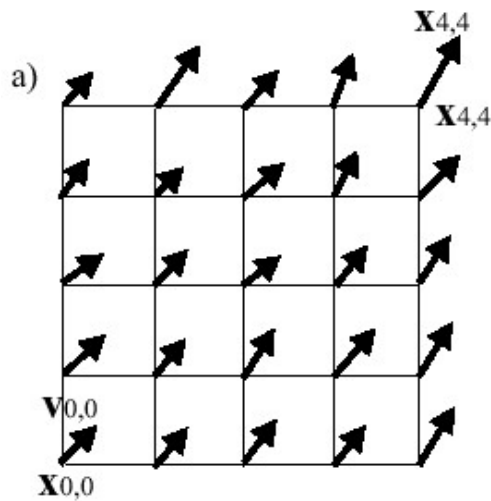


Eulerian

- Flow properties given at fixed spatial positions (grid points)
- Partial time derivative

Lagrangian

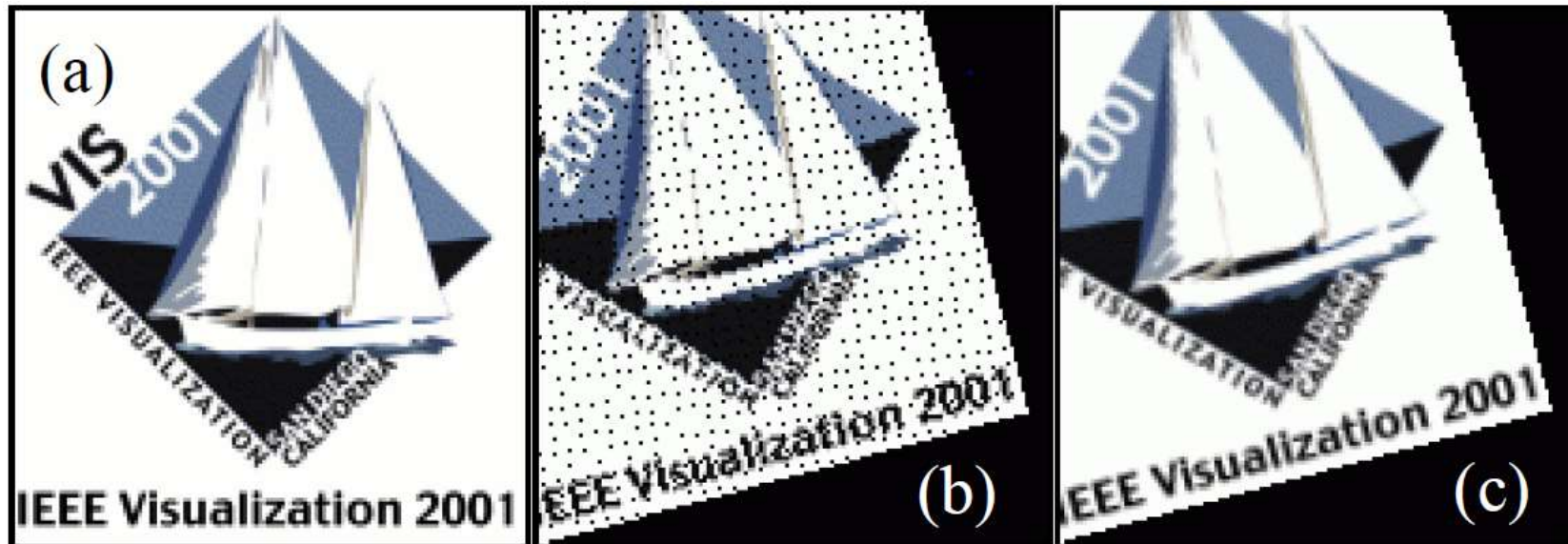
- Flow properties given for each particle (particles are moving)
- Material time derivative



Lagrangian vs. Eulerian



- Lagrangian: move along with the particle
- Eulerian: consider fixed point in space, look at particles moving through



- Example for pixels: rotate image (a),
Lagrangian: move pixels forward (b),
Eulerian: fetch pixels from backward direction (c)

Material Derivative (1)



The material time derivative (convective derivative) gives the rate of change when following a particle in the flow

$$\frac{D}{Dt} = \frac{\partial}{\partial t} + (\mathbf{u} \cdot \nabla)$$

Material Derivative (1)



The material time derivative (convective derivative) gives the rate of change when following a particle in the flow

$$\frac{D}{Dt} = \frac{\partial}{\partial t} + (\mathbf{u} \cdot \nabla)$$

$$\frac{DT}{Dt} = \frac{\partial T}{\partial t} + (\mathbf{u} \cdot \nabla) T$$

Material Derivative (1)



The material time derivative (convective derivative) gives the rate of change when following a particle in the flow

$$\frac{D}{Dt} = \frac{\partial}{\partial t} + (\mathbf{u} \cdot \nabla)$$

$$\frac{DT}{Dt} = \frac{\partial T}{\partial t} + (\mathbf{u} \cdot \nabla) T$$

$$\frac{DT}{Dt} = \frac{\partial T}{\partial t} + u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} + w \frac{\partial T}{\partial z}$$

Material Derivative (2)



Actually, nothing else than application of the multi-variable chain rule:

$$dT = \frac{\partial T}{\partial t} dt + \frac{\partial T}{\partial x} dx + \frac{\partial T}{\partial y} dy + \frac{\partial T}{\partial z} dz$$

Material Derivative (2)



Actually, nothing else than application of the multi-variable chain rule:

$$dT = \frac{\partial T}{\partial t} dt + \frac{\partial T}{\partial x} dx + \frac{\partial T}{\partial y} dy + \frac{\partial T}{\partial z} dz$$

$$dT = \frac{\partial T}{\partial t} dt + \frac{\partial T}{\partial x} \frac{dx}{dt} dt + \frac{\partial T}{\partial y} \frac{dy}{dt} dt + \frac{\partial T}{\partial z} \frac{dz}{dt} dt$$

Material Derivative (2)



Actually, nothing else than application of the multi-variable chain rule:

$$dT = \frac{\partial T}{\partial t} dt + \frac{\partial T}{\partial x} dx + \frac{\partial T}{\partial y} dy + \frac{\partial T}{\partial z} dz$$

$$dT = \frac{\partial T}{\partial t} dt + \frac{\partial T}{\partial x} \frac{dx}{dt} dt + \frac{\partial T}{\partial y} \frac{dy}{dt} dt + \frac{\partial T}{\partial z} \frac{dz}{dt} dt$$

$$\frac{dT}{dt} = \frac{\partial T}{\partial t} + \frac{\partial T}{\partial x} \frac{dx}{dt} + \frac{\partial T}{\partial y} \frac{dy}{dt} + \frac{\partial T}{\partial z} \frac{dz}{dt}$$

Material Derivative (2)



Actually, nothing else than application of the multi-variable chain rule:

$$dT = \frac{\partial T}{\partial t} dt + \frac{\partial T}{\partial x} dx + \frac{\partial T}{\partial y} dy + \frac{\partial T}{\partial z} dz$$

$$dT = \frac{\partial T}{\partial t} dt + \frac{\partial T}{\partial x} \frac{dx}{dt} dt + \frac{\partial T}{\partial y} \frac{dy}{dt} dt + \frac{\partial T}{\partial z} \frac{dz}{dt} dt$$

$$\frac{dT}{dt} = \frac{\partial T}{\partial t} + \frac{\partial T}{\partial x} \frac{dx}{dt} + \frac{\partial T}{\partial y} \frac{dy}{dt} + \frac{\partial T}{\partial z} \frac{dz}{dt}$$

$$u := \frac{dx}{dt}, \quad v := \frac{dy}{dt}, \quad w := \frac{dz}{dt}$$

Material Derivative (2)



Actually, nothing else than application of the multi-variable chain rule:

We are given $T(x, y, z, t)$ with four independent variables;

But now we want to go along a parameterized path with parameter t ,
so x, y, z become dependent variables: $x(t), y(t), z(t)$

Along this path, our goal is now to compute the derivative of the function

$T(x(t), y(t), z(t), t)$ with t as only independent variable:

$$\frac{d}{dt}T(x(t), y(t), z(t), t) = \frac{\partial}{\partial t}T(x, y, z, t) + \frac{\partial}{\partial x}T(x, y, z, t) \frac{d}{dt}x(t) + \frac{\partial}{\partial y}T(x, y, z, t) \frac{d}{dt}y(t) + \frac{\partial}{\partial z}T(x, y, z, t) \frac{d}{dt}z(t)$$

$$u(t) := \frac{dx(t)}{dt}, \quad v(t) := \frac{dy(t)}{dt}, \quad w(t) := \frac{dz(t)}{dt}$$

Advection



Advection equation; velocity field $\mathbf{u}(x, y, z, t)$,
no change following particle, just advection:
set material derivative = 0:

$$\frac{\partial T}{\partial t} + (\mathbf{u} \cdot \nabla) T = 0$$

In the Navier-Stokes equations: “self-advection” of velocity

- Advect scalar components of velocity field individually
(actually two equations in 2D, three equations in 3D)

$$\frac{\partial \mathbf{u}}{\partial t} = -(\mathbf{u} \cdot \nabla) \mathbf{u}$$

this is equivalent to
saying that the
acceleration is zero!

Vector Fields and Dynamical Systems (1)



Velocity gradient tensor, (vector field \rightarrow tensor field)

- Gradient of vector field: how does the vector field change?
- In Cartesian coordinates: *spatial partial derivatives (Jacobian matrix)*

$$\nabla \mathbf{v} (x, y, z) = \begin{pmatrix} u_x & u_y & u_z \\ v_x & v_y & v_z \\ w_x & w_y & w_z \end{pmatrix} \quad \text{these are partial derivatives!}$$

- Can be decomposed into *symmetric* part + *anti-symmetric* part

$$\nabla \mathbf{v} = \mathbf{D} + \mathbf{S} \quad \text{velocity gradient tensor}$$

$$\text{sym.:} \quad \mathbf{D} = \frac{1}{2} (\nabla \mathbf{v} + (\nabla \mathbf{v})^T) \quad \text{deform.:} \quad \textit{rate-of-strain tensor}$$

$$\text{skew-sym.:} \quad \mathbf{S} = \frac{1}{2} (\nabla \mathbf{v} - (\nabla \mathbf{v})^T) \quad \text{rotation:} \quad \textit{vorticity/spin tensor}$$

Vector Fields and Dynamical Systems (2)



Vorticity/spin/angular velocity tensor

- Antisymmetric part of velocity gradient tensor
- Corresponds to vorticity/curl/angular velocity (beware of factor $\frac{1}{2}$)

$$\mathbf{S} = \frac{1}{2} (\nabla \mathbf{v} - (\nabla \mathbf{v})^T)$$

these are
partial
derivatives!

$$\mathbf{S} = \frac{1}{2} \begin{pmatrix} 0 & -\omega_3 & \omega_2 \\ \omega_3 & 0 & -\omega_1 \\ -\omega_2 & \omega_1 & 0 \end{pmatrix} \quad \boldsymbol{\omega} = \begin{pmatrix} \omega_1 \\ \omega_2 \\ \omega_3 \end{pmatrix} = \nabla \times \mathbf{v} = \begin{pmatrix} w_y - v_z \\ u_z - w_x \\ v_x - u_y \end{pmatrix}$$

\mathbf{S} acts on vector like cross product with $\boldsymbol{\omega}$: $\mathbf{S} \cdot \mathbf{v} = \frac{1}{2} \boldsymbol{\omega} \times \mathbf{v}$

$$\mathbf{v}^{(r)} = \mathbf{S} \cdot d\mathbf{r} = \frac{1}{2} [\nabla \mathbf{v} - (\nabla \mathbf{v})^T] \cdot d\mathbf{r} = \frac{1}{2} \boldsymbol{\omega} \times d\mathbf{r}$$

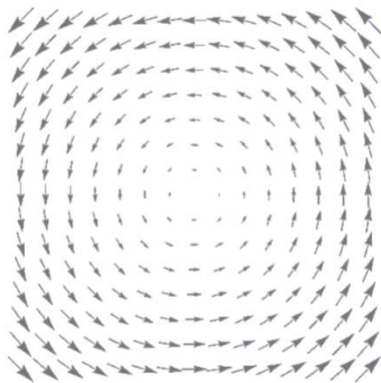
Angular Velocity of Rigid Body Rotation



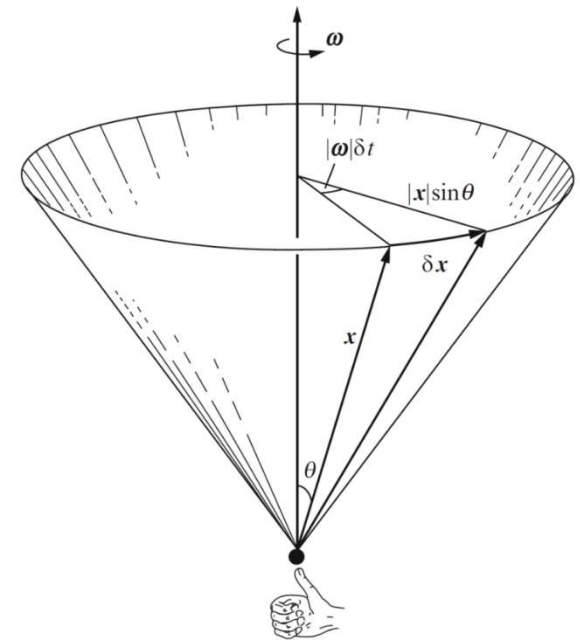
Rate of rotation

- Scalar ω : angular displacement per unit time (rad s^{-1})
 - Angle Θ at time t is $\Theta(t) = \omega t$; $\omega = 2\pi f$ where f is the frequency ($f = 1/T$; s^{-1})
- Vector $\boldsymbol{\omega}$: axis of rotation; magnitude is angular speed (if $\boldsymbol{\omega}$ is curl: speed $\times 2$)
 - Beware of different conventions that differ by a factor of $\frac{1}{2}$!

Cross product of $\frac{1}{2}\boldsymbol{\omega}$ with vector to center of rotation (\mathbf{r}) gives linear velocity vector \mathbf{v} (tangent)



$$\mathbf{v}^{(r)} = \frac{1}{2} \boldsymbol{\omega} \times d\mathbf{r}$$



Velocity Gradient Tensor and Components (1)



Velocity gradient tensor

(here: in Cartesian coordinates)

$$\nabla \mathbf{v} = \begin{bmatrix} \frac{\partial}{\partial x} v^x & \frac{\partial}{\partial y} v^x & \frac{\partial}{\partial z} v^x \\ \frac{\partial}{\partial x} v^y & \frac{\partial}{\partial y} v^y & \frac{\partial}{\partial z} v^y \\ \frac{\partial}{\partial x} v^z & \frac{\partial}{\partial y} v^z & \frac{\partial}{\partial z} v^z \end{bmatrix}$$

these are the same
partial derivatives
as before!

$$\nabla \mathbf{v} = \frac{1}{2} \left(\nabla \mathbf{v} + (\nabla \mathbf{v})^T \right) + \frac{1}{2} \left(\nabla \mathbf{v} - (\nabla \mathbf{v})^T \right)$$

Velocity Gradient Tensor and Components (2)



Rate-of-strain (rate-of-deformation) tensor

(symmetric part; here: in Cartesian coordinates)

$$\mathbf{D} = \frac{1}{2} \begin{bmatrix} 2 \frac{\partial}{\partial x} v^x & \frac{\partial}{\partial y} v^x + \frac{\partial}{\partial x} v^y & \frac{\partial}{\partial z} v^x + \frac{\partial}{\partial x} v^z \\ \frac{\partial}{\partial x} v^y + \frac{\partial}{\partial y} v^x & 2 \frac{\partial}{\partial y} v^y & \frac{\partial}{\partial z} v^y + \frac{\partial}{\partial y} v^z \\ \frac{\partial}{\partial x} v^z + \frac{\partial}{\partial z} v^x & \frac{\partial}{\partial y} v^z + \frac{\partial}{\partial z} v^y & 2 \frac{\partial}{\partial z} v^z \end{bmatrix}$$

$$tr(\mathbf{D}) = \nabla \cdot \mathbf{v}$$

Velocity Gradient Tensor and Components (3)



Vorticity tensor (spin tensor)

(skew-symmetric part; here: in Cartesian coordinates)

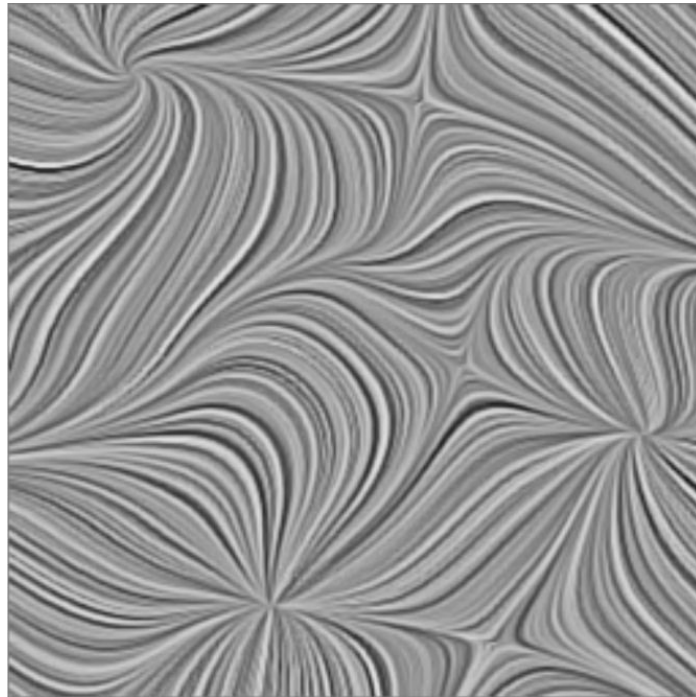
$$\mathbf{S} = \frac{1}{2} \begin{bmatrix} 0 & \frac{\partial}{\partial y} v^x - \frac{\partial}{\partial x} v^y & \frac{\partial}{\partial z} v^x - \frac{\partial}{\partial x} v^z \\ \frac{\partial}{\partial x} v^y - \frac{\partial}{\partial y} v^x & 0 & \frac{\partial}{\partial z} v^y - \frac{\partial}{\partial y} v^z \\ \frac{\partial}{\partial x} v^z - \frac{\partial}{\partial z} v^x & \frac{\partial}{\partial y} v^z - \frac{\partial}{\partial z} v^y & 0 \end{bmatrix}$$

$$\mathbf{S} = \frac{1}{2} \begin{bmatrix} 0 & -\omega_z & \omega_y \\ \omega_z & 0 & -\omega_x \\ -\omega_y & \omega_x & 0 \end{bmatrix} \quad \boldsymbol{\omega} \equiv \nabla \times \mathbf{v}$$

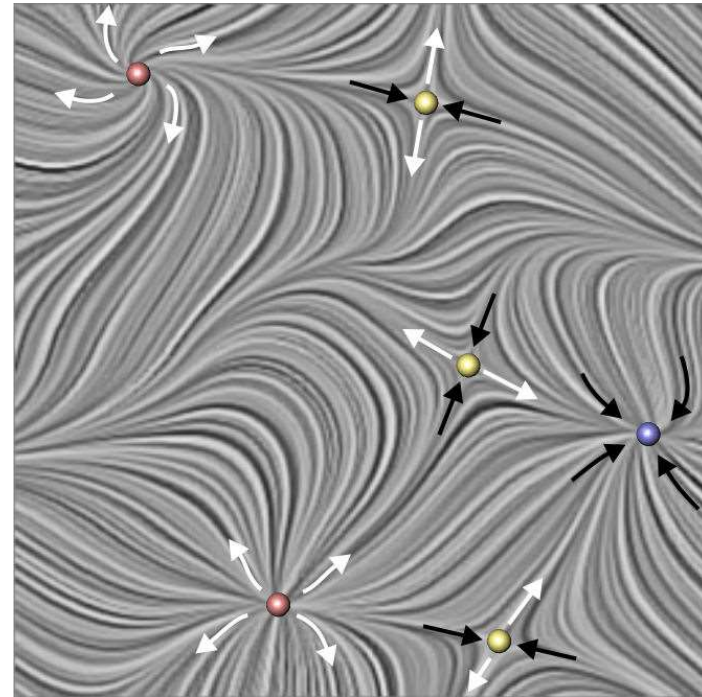
Critical Points (Steady Flow!)



Classify critical points according to the *eigenvalues* of the velocity gradient tensor at the critical point



stream lines (LIC)



critical points ($\mathbf{v} = 0$)

(Non-Linear) Dynamical Systems



Start with system of linear ODEs (with constant coefficients)

- Non-linear systems can be linearized around critical points
- Use linearization for characterization

$$\dot{\mathbf{x}} = A\mathbf{x}$$

A is an $n \times n$ matrix



$$\begin{aligned} \mathbf{v} &= A\mathbf{x}, \\ \nabla \mathbf{v} &= A. \end{aligned}$$

$$\dot{\mathbf{x}} = \frac{d\mathbf{x}}{dt} = \begin{bmatrix} \frac{dx_1}{dt} \\ \vdots \\ \frac{dx_n}{dt} \end{bmatrix}$$

$$\mathbf{x}(0) = \mathbf{x}_0$$

solution: $\mathbf{x}(t) = e^{At}\mathbf{x}_0$

characterize behavior
through eigenvalues of A

A Few Facts about Eigenvalues and –vectors



The matrix $\begin{bmatrix} c & -s \\ s & c \end{bmatrix}$ has eigenvalues $\lambda_1 = c + si$ $\lambda_2 = c - si$
with eigenvectors $u_1 = \begin{bmatrix} 1 \\ -i \end{bmatrix}$ $u_2 = \begin{bmatrix} 1 \\ +i \end{bmatrix}$

If $c = 0$, this is a skew-symmetric matrix

Skew-symmetric matrices: “infinitesimal rotations” (infinitesimal generators of rot.)

For $c = \cos \theta$ and $s = \sin \theta$: 2x2 rotation matrix with $\lambda_1 = e^{i\theta} = \cos \theta + i \sin \theta$
 $\lambda_2 = e^{-i\theta} = \cos \theta - i \sin \theta$

Eigenvalues

- Symmetric matrix: all eigenvalues are *real*
- Skew-symmetric matrix: all eigenvalues are *pure imaginary*

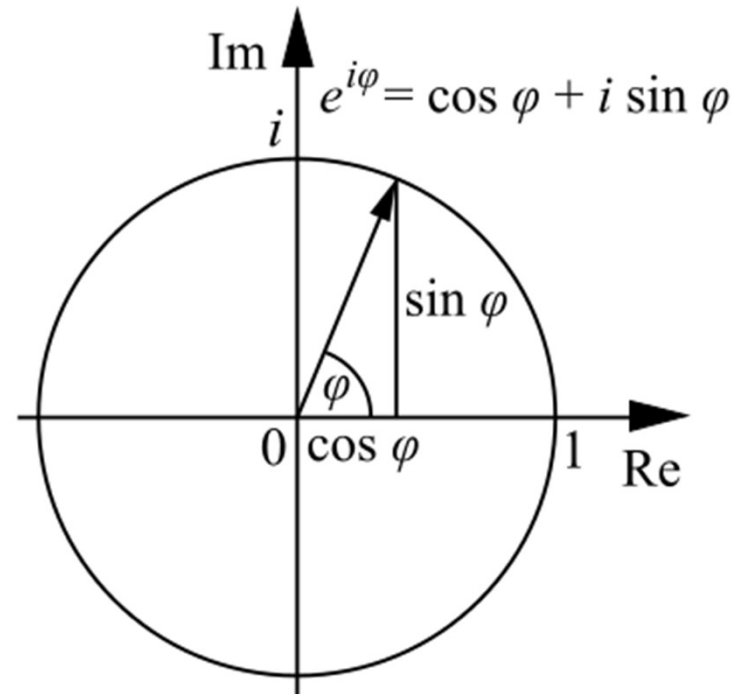
Euler's Formula



Can be derived from the infinite power series for $\exp()$, $\cos()$, $\sin()$

$$e^{ix} = \cos x + i \sin x$$

$$e^{i\pi} + 1 = 0$$



Matrix Exponentials



Defined via same power series as usual exponential

$$\exp(X) = e^X := \sum_{k=0}^{\infty} \frac{X^k}{k!} = I + X + \frac{X^2}{2!} + \frac{X^3}{3!} + \dots$$

Easy if X is diagonalizable

$$X = \begin{pmatrix} \lambda_1 & 0 \\ 0 & \lambda_2 \end{pmatrix} \quad \exp(X) = \begin{pmatrix} e^{\lambda_1} & 0 \\ 0 & e^{\lambda_2} \end{pmatrix}$$

Exponentials of anti-symmetric matrices are rotation matrices

$$X = \begin{pmatrix} 0 & -1 \\ 1 & 0 \end{pmatrix} \quad \exp(tX) = \begin{pmatrix} \cos t & -\sin t \\ \sin t & \cos t \end{pmatrix}$$

Matrix Exponentials



Defined via same power series as usual exponential

$$\exp(X) = e^X := \sum_{k=0}^{\infty} \frac{X^k}{k!} = I + X + \frac{X^2}{2!} + \frac{X^3}{3!} + \dots$$

Easy if X is diagonalizable

$$X = \begin{pmatrix} \lambda_1 & 0 \\ 0 & \lambda_2 \end{pmatrix} \quad \exp(tX) = \begin{pmatrix} e^{\lambda_1 t} & 0 \\ 0 & e^{\lambda_2 t} \end{pmatrix}$$

Exponentials of anti-symmetric matrices are rotation matrices

$$X = \begin{pmatrix} 0 & -1 \\ 1 & 0 \end{pmatrix} \quad \exp(tX) = \begin{pmatrix} \cos t & -\sin t \\ \sin t & \cos t \end{pmatrix}$$

Matrix Exponentials



Defined via same power series as usual exponential

$$\exp(X) = e^X := \sum_{k=0}^{\infty} \frac{X^k}{k!} = I + X + \frac{X^2}{2!} + \frac{X^3}{3!} + \dots$$

Easy if X is diagonalizable

$$X = \begin{pmatrix} \lambda_1 & 0 \\ 0 & \lambda_2 \end{pmatrix} \quad \exp(tX) = \begin{pmatrix} e^{\lambda_1 t} & 0 \\ 0 & e^{\lambda_2 t} \end{pmatrix}$$

Complex eigenvalues lead to rotation

$$X = \begin{pmatrix} a & -\omega \\ \omega & a \end{pmatrix} \quad \exp(tX) = \begin{pmatrix} \operatorname{Re}(e^{\lambda t}) & -\operatorname{Im}(e^{\lambda t}) \\ \operatorname{Im}(e^{\lambda t}) & \operatorname{Re}(e^{\lambda t}) \end{pmatrix}$$

$$\lambda_{1,2} = a \pm \mathbf{i}\omega$$

Matrix Exponentials



Defined via same power series as usual exponential

$$\exp(X) = e^X := \sum_{k=0}^{\infty} \frac{X^k}{k!} = I + X + \frac{X^2}{2!} + \frac{X^3}{3!} + \dots$$

Easy if X is diagonalizable

$$X = \begin{pmatrix} \lambda_1 & 0 \\ 0 & \lambda_2 \end{pmatrix} \quad \exp(tX) = \begin{pmatrix} e^{\lambda_1 t} & 0 \\ 0 & e^{\lambda_2 t} \end{pmatrix}$$

Complex eigenvalues lead to rotation

$$X = \begin{pmatrix} a & -\omega \\ \omega & a \end{pmatrix} \quad \exp(tX) = e^{at} \begin{pmatrix} \cos \omega t & -\sin \omega t \\ \sin \omega t & \cos \omega t \end{pmatrix}$$

$$\lambda_{1,2} = a \pm \mathbf{i}\omega$$

Classification of Critical Points



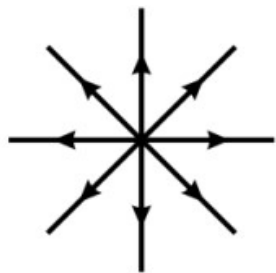
(Isolated) critical point (equilibrium point)

- Velocity vanishes (all components zero)

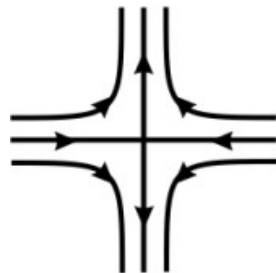
$$\mathbf{v}(\mathbf{x}_c) = \mathbf{0} \quad \text{with} \quad \mathbf{v}(\mathbf{x}_c \pm \epsilon) \neq \mathbf{0} \quad \det(\nabla \mathbf{v}(\mathbf{x}_c)) \neq 0$$

Characterize using velocity gradient $\nabla \mathbf{v}$ at critical point \mathbf{x}_c

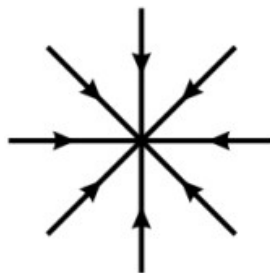
- Look at eigenvalues (and eigenvectors) of $\nabla \mathbf{v}$



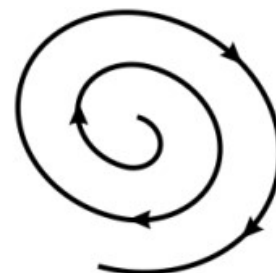
Repelling node
 $R_1, R_2 > 0$
 $I_1 = I_2 = 0$



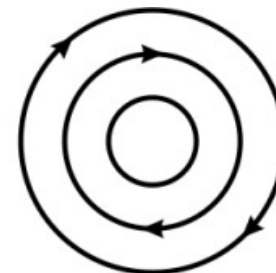
Saddle point
 $R_1 < 0, R_2 > 0$
 $I_1 = I_2 = 0$



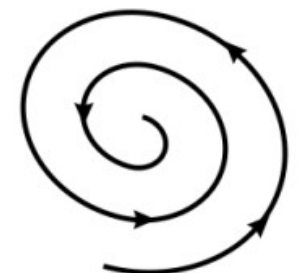
Attracting node
 $R_1, R_2 < 0$
 $I_1 = I_2 = 0$



Repelling focus
 $R_1 = R_2 > 0$
 $I_1 = -I_2 \neq 0$



Center
 $R_1 = R_2 = 0$
 $I_1 = -I_2 \neq 0$



Attracting focus
 $R_1 = R_2 < 0$
 $I_1 = -I_2 \neq 0$

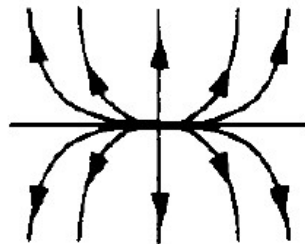
the first three phase portraits are special cases, see later slides!

A Few Details (1)



Repelling/attracting nodes

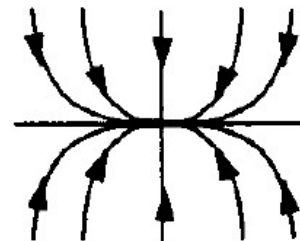
- Do not necessarily imply that streamlines are straight lines (do not confuse with the linear system of ODEs!)
- They are only straight lines when both eigenvalues are real and have the same sign, *and are also equal* (as in the phase portraits before)
- If they are not equal:



Repelling Node

$$R_1, R_2 > 0$$

$$I_1, I_2 = 0$$



Attracting Node

$$R_1, R_2 < 0$$

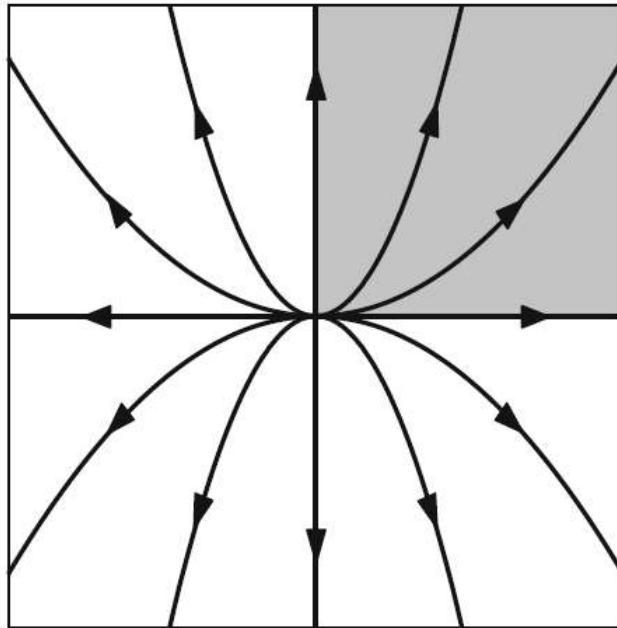
$$I_1, I_2 = 0$$

A Few Details (2)

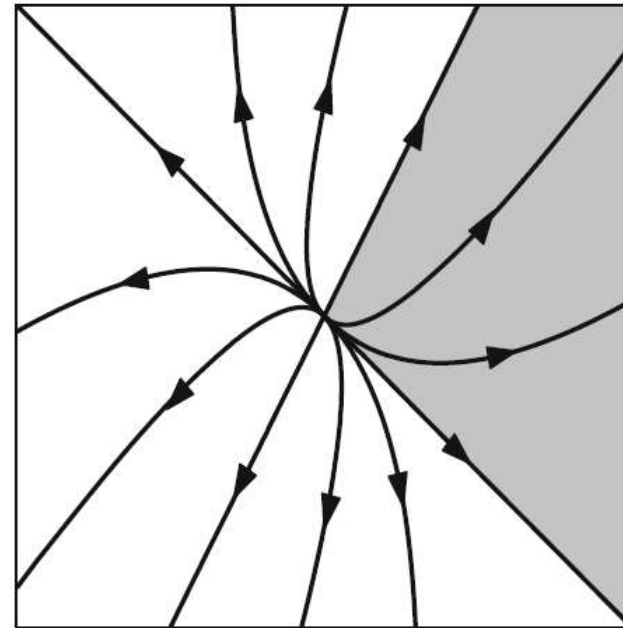


What about skew axes?

- Both of the systems below have eigenvalues 3 and 6
- Jordan normal form (Jordan canonical form) gives details



$$\begin{bmatrix} 3 & 0 \\ 0 & 6 \end{bmatrix}$$



$$\begin{bmatrix} 4 & 1 \\ 2 & 5 \end{bmatrix}$$

Jordan Normal Form (2x2 Matrix)



For every real 2x2 matrix A there is an invertible P such that

$P^{-1}AP$ is one of the following Jordan matrices (all entries are real):

$$J_1 = \begin{bmatrix} \lambda_1 & 0 \\ 0 & \lambda_2 \end{bmatrix} \quad J_2 = \begin{bmatrix} \lambda & 0 \\ 1 & \lambda \end{bmatrix} \quad (\text{defective matrix})$$

$$J_3 = \begin{bmatrix} \lambda & 0 \\ 0 & \lambda \end{bmatrix} \quad J_4 = \begin{bmatrix} a & -b \\ b & a \end{bmatrix}$$

Each of these has its corresponding rule for constructing P

- Example on prev. slide (the two eigenvectors are not orthogonal):

$$P = \frac{1}{3} \begin{bmatrix} 1 & 1 \\ -1 & 2 \end{bmatrix} \quad \frac{1}{3} \begin{bmatrix} 2 & -1 \\ 1 & 1 \end{bmatrix} \begin{bmatrix} 4 & 1 \\ 2 & 5 \end{bmatrix} \begin{bmatrix} 1 & 1 \\ -1 & 2 \end{bmatrix} = \begin{bmatrix} 3 & 0 \\ 0 & 6 \end{bmatrix}$$

See also *algebraic* and *geometric multiplicity* of eigenvalues

Another Example



$P^{-1}AP$ has form J_1

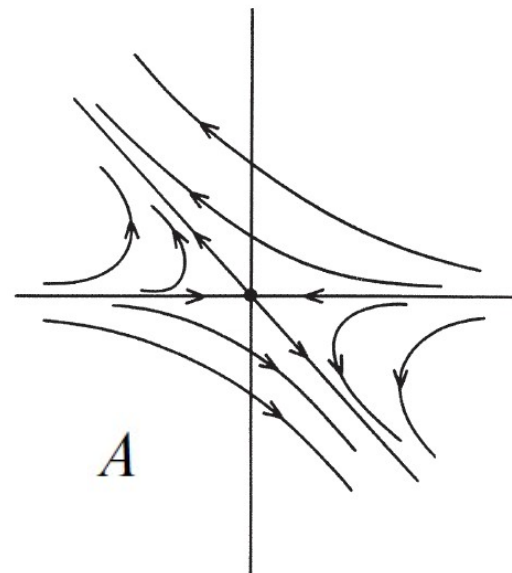
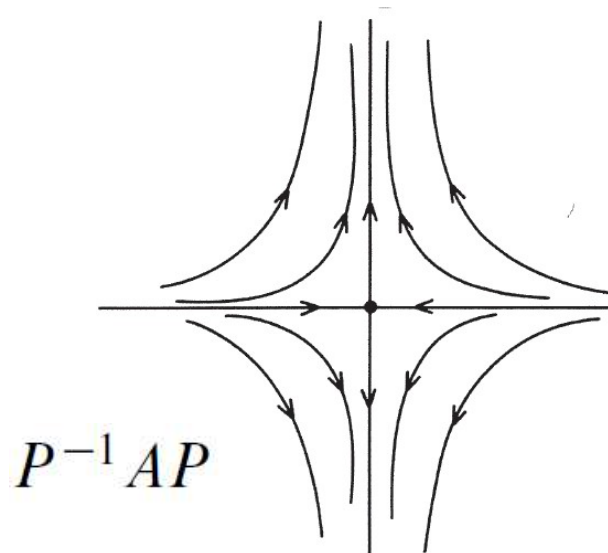
Eigenvalues:

$$\lambda_1 = -1$$

$$\lambda_2 = 2$$

$$A = \begin{bmatrix} -1 & -3 \\ 0 & 2 \end{bmatrix}$$

$$P = \begin{bmatrix} 1 & -1 \\ 0 & 1 \end{bmatrix} \quad P^{-1} = \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix}$$

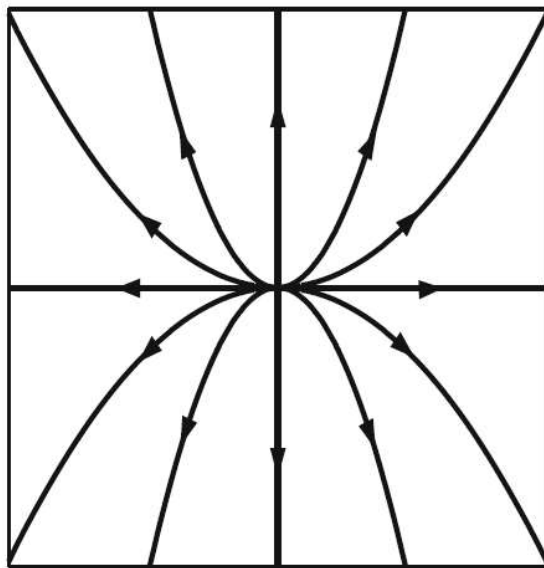


Jordan Form Characterization (1)

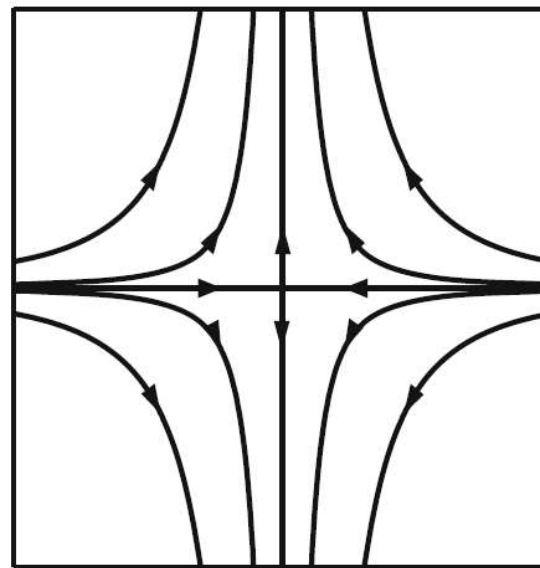


Phase portraits corresponding to Jordan matrix

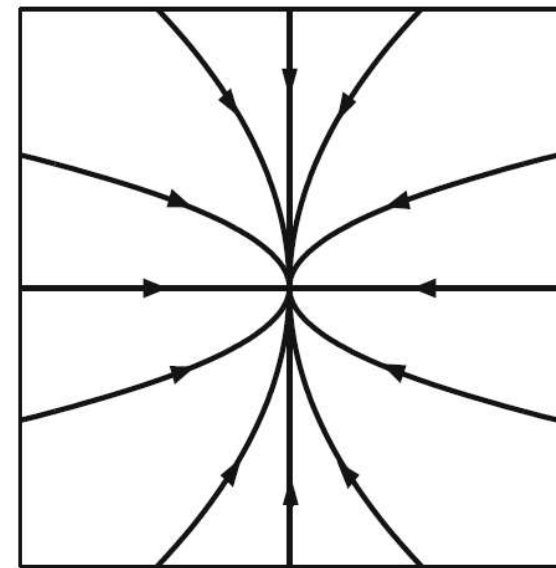
$$J_1 = \begin{bmatrix} \lambda_1 & 0 \\ 0 & \lambda_2 \end{bmatrix}$$



$0 < \lambda_1 < \lambda_2$
unstable node



$\lambda_1 < 0 < \lambda_2$
saddle



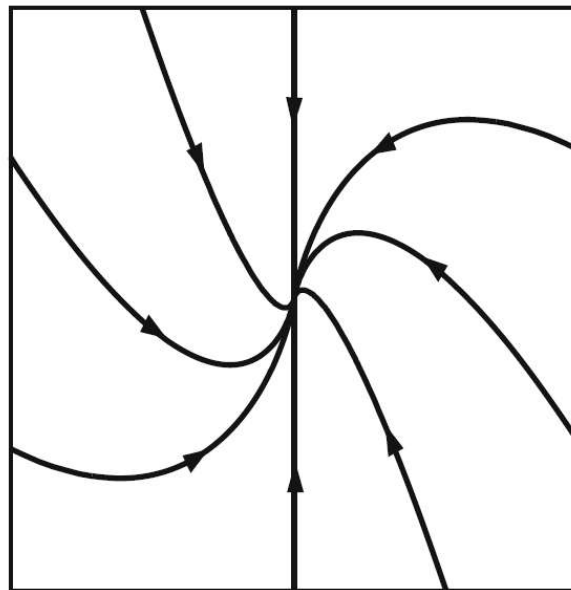
$\lambda_1 < \lambda_2 < 0$
stable node

Jordan Form Characterization (2)



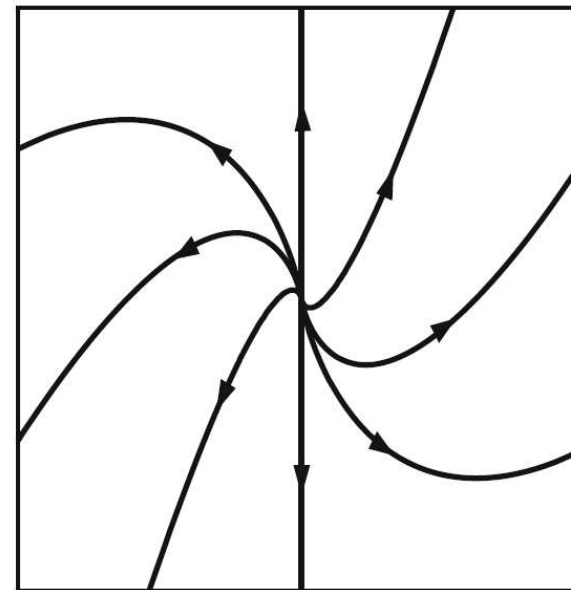
Phase portraits corresponding to Jordan matrix

$$J_2 = \begin{bmatrix} \lambda & 0 \\ 1 & \lambda \end{bmatrix}$$



$$\lambda < 0$$

stable improper node



$$\lambda > 0$$

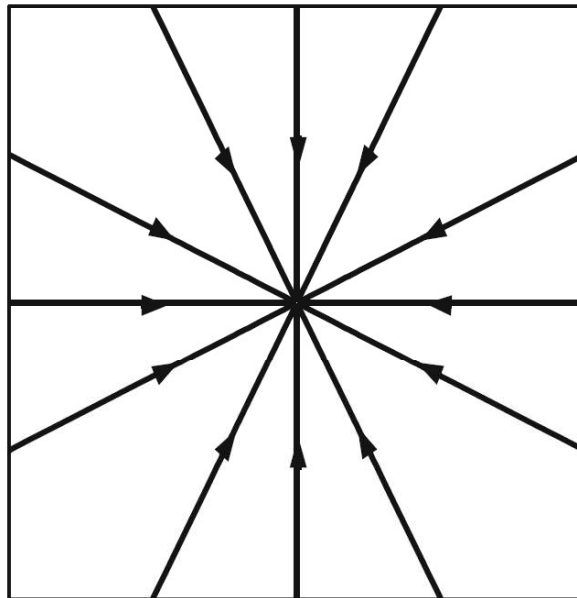
unstable improper node

Jordan Form Characterization (3)

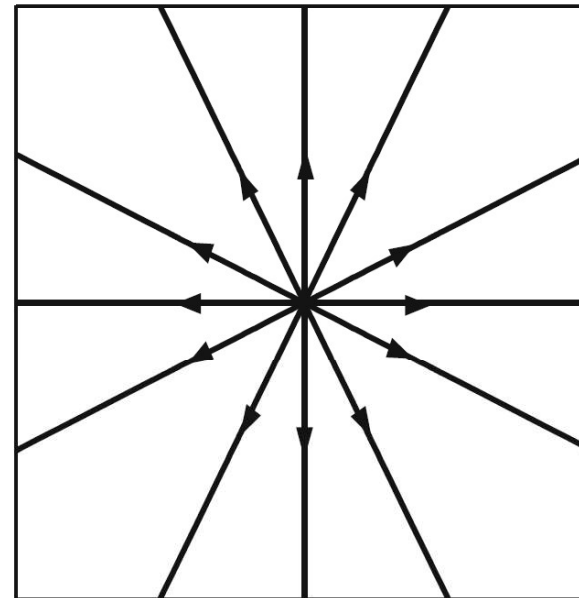


Phase portraits corresponding to Jordan matrix

$$J_3 = \begin{bmatrix} \lambda & 0 \\ 0 & \lambda \end{bmatrix}$$



$\lambda < 0$
stable star node



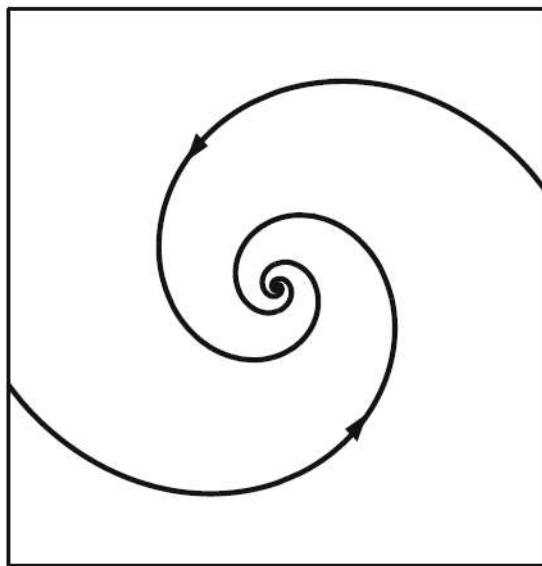
$\lambda > 0$
unstable star node

Jordan Form Characterization (4)

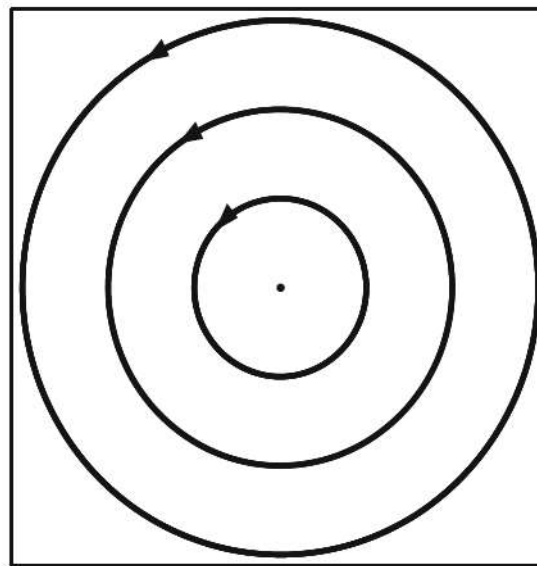


Phase portraits corresponding to Jordan matrix

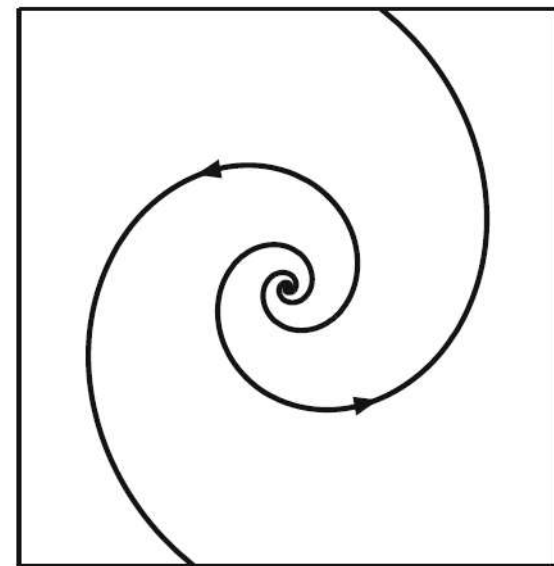
$$J_4 = \begin{bmatrix} a & -b \\ b & a \end{bmatrix}$$



$a < 0$
stable spiral node



$a = 0$
center

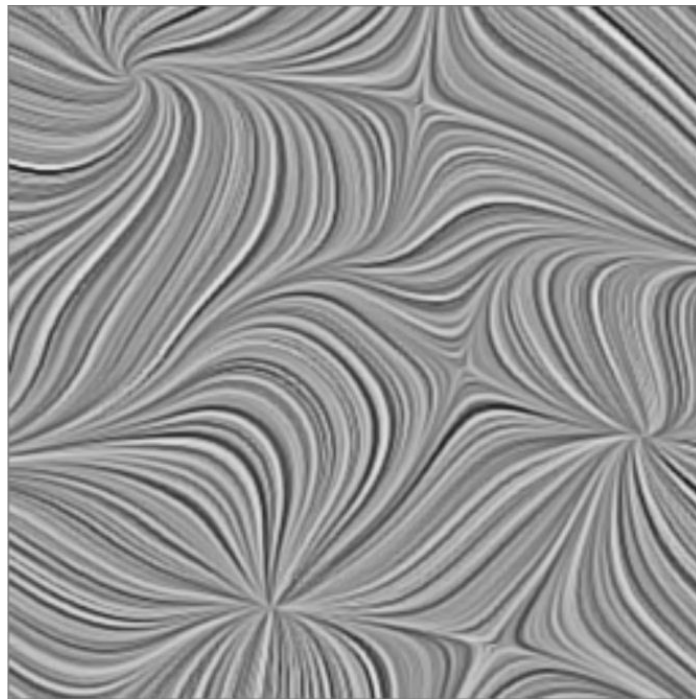


$a > 0$
unstable spiral node

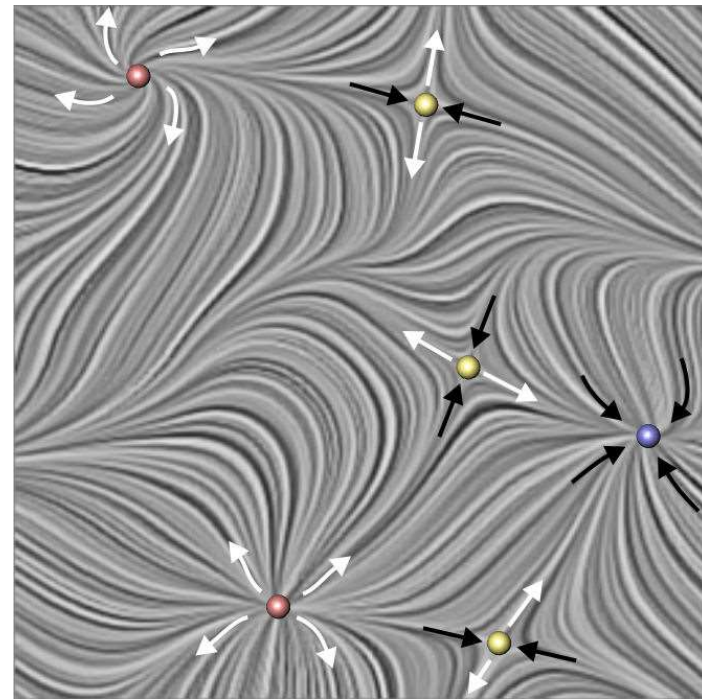
Critical Points (Steady Flow!)



Classify critical points according to the *eigenvalues* of the velocity gradient tensor at the critical point

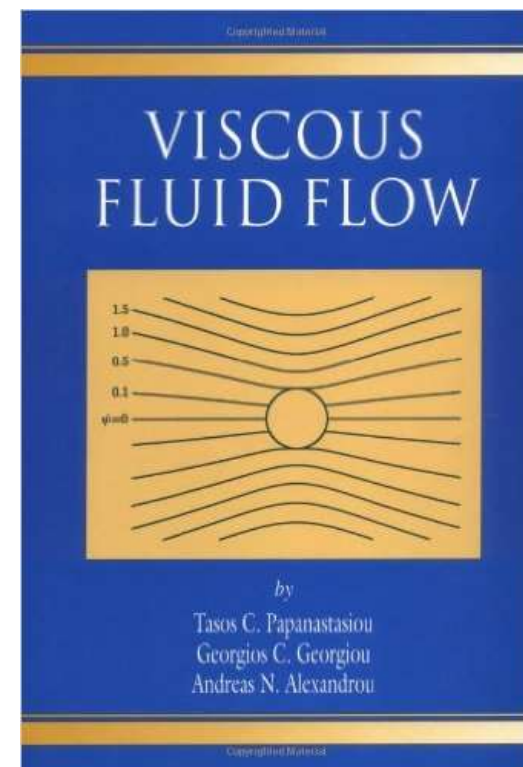
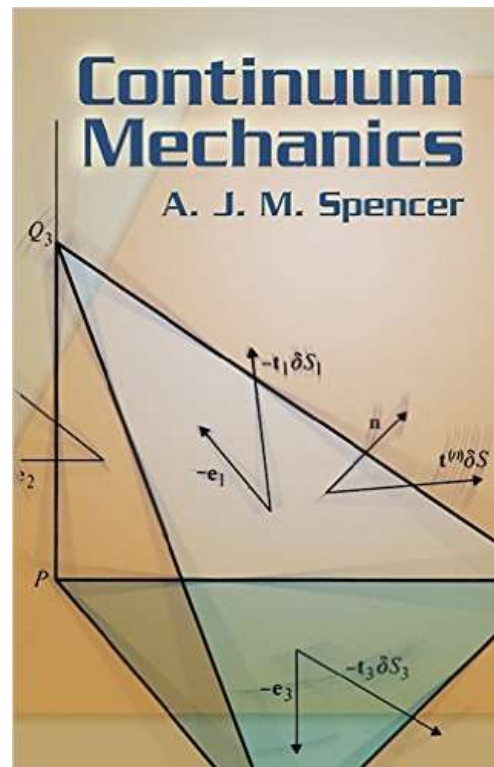
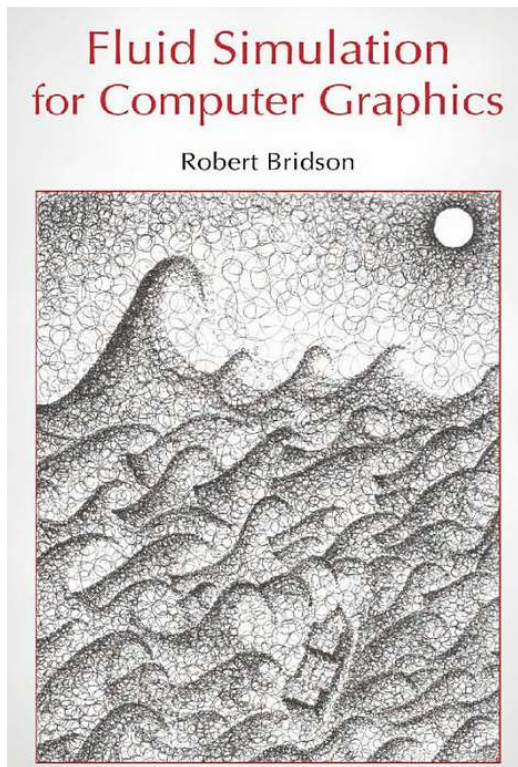


stream lines (LIC)

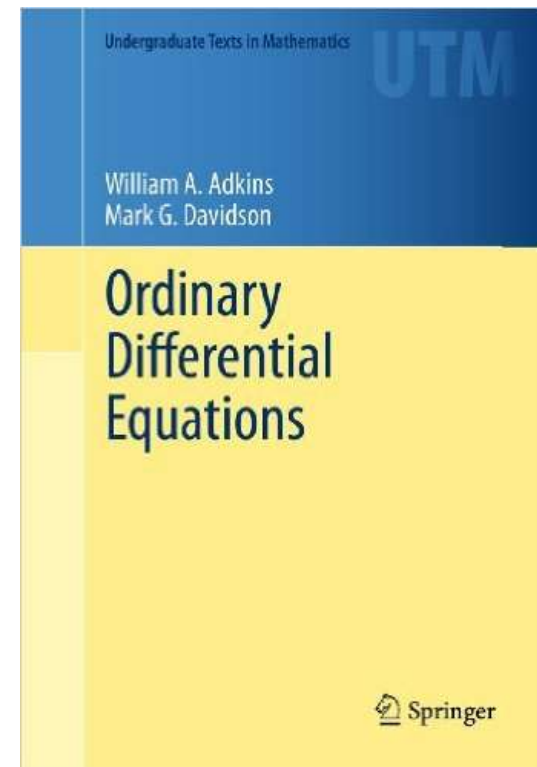
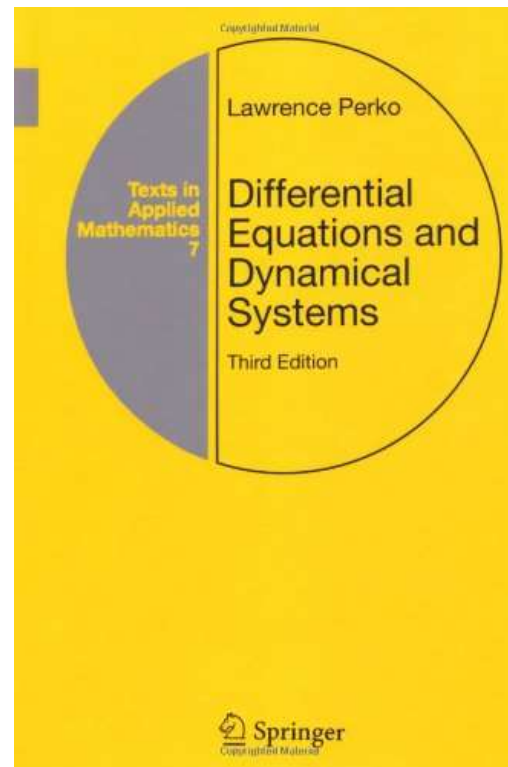


critical points ($\mathbf{v} = 0$)

Recommended Books (1)



Recommended Books (2)



Thank you.

Thanks for material

- Helwig Hauser
- Eduard Gröller
- Daniel Weiskopf
- Torsten Möller
- Ronny Peikert
- Philipp Muigg
- Christof Rezk-Salama